

AD-A271 756



2

ARMY RESEARCH LABORATORY



Investigation of the Effect of Various Oxide and Flouride Additives on the Microstructure, Electronic Properties, and Phase Shifting Ability of $\text{Ba}_{1-x}\text{Sr}_x\text{TiO}_3$

L.C. Sengupta, E. Ngo, S. Stowell, R. Lancto, W.C. Drach,
T.E. Koscica, and R.W. Babbitt

ARL-TR-217

September 1993

DTIC
ELECTE
NOV 03 1993
S B D

93-26410



Approved for public release; distribution unlimited

93 11 1 063

**Best
Available
Copy**

The findings in this report are not to be construed as an official Department of the Army position unless so designated by other authorized documents.

Citation of manufacturer's or trade names does not constitute an official endorsement or approval of the use thereof.

Destroy this report when it is no longer needed. Do not return it to the originator.

REPORT DOCUMENTATION PAGE			Form Approved OMB No. 0704-0188	
<small>P. One reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (0704-0188), Washington, DC 20503.</small>				
1. AGENCY USE ONLY (Leave blank)		2. REPORT DATE September 1993		3. REPORT TYPE AND DATES COVERED Final Report
4. TITLE AND SUBTITLE Investigation of the Effect of Various Oxide and Fluoride Additives on the Microstructure, Electronic Properties, and Phase Shifting Ability of $Ba_{1-x}Sr_xTiO_3$			5. FUNDING NUMBERS	
6. AUTHOR(S) L. C. Sengupta, E. Ngo, S. Stowell, and R. Lancto W. C. Drach,* T. E. Koscica,* and R. W. Babbitt*				
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) U.S. Army Research Laboratory Watertown, MA 02172-0001 ATTN: AMSRL-MA-CA			8. PERFORMING ORGANIZATION REPORT NUMBER ARL-TR-217	
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES) U.S. Army Research Laboratory 2800 Powder Mill Road Adelphi, MD 20783-1145			10. SPONSORING/MONITORING AGENCY REPORT NUMBER	
11. SUPPLEMENTARY NOTES *U.S. Army Research Laboratory Fort Monmouth, NJ 07703 ATTN: AMSRL-EP-M				
12a. DISTRIBUTION/AVAILABILITY STATEMENT Approved for public release; distribution unlimited.			12b. DISTRIBUTION CODE	
13. ABSTRACT (Maximum 200 words) A ceramic phase shifting device (used in phased array antenna systems) has been demonstrated using $Ba_{1-x}Sr_xTiO_3$ (BSTO) ceramics. As a part of an effort to optimize the electronic device performance in the phase shifter, various dopants have been incorporated into BSTO. The effects of these additives on the Curie temperature, dielectric properties, tunability, hysteresis, and grain size have been investigated. The homogeneity of the doped materials has been verified using Curie-Weiss analysis. To further improve the electrical performance, some higher levels of doping have been attempted. A few of the latest results for these ceramic-ceramic composites will be presented.				
14. SUBJECT TERMS Phased array antennas, Ferroelectrics, Electro-ceramics, Barium strontium titanate			15. NUMBER OF PAGES 26	
			16. PRICE CODE	
17. SECURITY CLASSIFICATION OF REPORT Unclassified	18. SECURITY CLASSIFICATION OF THIS PAGE Unclassified	19. SECURITY CLASSIFICATION OF ABSTRACT Unclassified	20. LIMITATION OF ABSTRACT UL	

Contents

	Page
Introduction	1
Experimental	
Ceramic Processing	1
Electronic Measurements	3
Results and Discussion	5
Conclusions	19
Acknowledgments	19
References	19

Figures

1. Block diagram of ARL-EPDS electronic test equipment	4
2. Specimen holder and heating apparatus for electronic test system	5
3. Curie-Weiss relationship $1/\epsilon$ versus temperature for: (a) an undoped specimen, and (b) a specimen doped with 2 wt% zirconia	6
4. Dielectric constant versus tunability (1.5 V/micron) for doped BSTO (Ba=0.75) ..	8
5. Curie temperature ($^{\circ}\text{C}$) versus % tunability (1.5 V/micron) for doped BSTO (Ba=0.75)	8
6. Dielectric constant versus grain size for doped BSTO (Ba=0.75)	9
7. Curie temperature and tunability (1.5 V/micron) versus grain size for doped BSTO (Ba=0.75)	9
8. Dielectric constant versus tunability (1.5 V/micron) for doped BTO	11
9. Curie temperature ($^{\circ}\text{C}$) versus % tunability (1.5 V/micron) for doped BTO	11
10. Dielectric constant versus grain size for doped BTO	13
11. Curie temperature and tunability (1.5 V/micron) versus grain size for doped BTO	13
12. Dielectric constant versus barium content, $\text{Ba}(1-x)$, for undoped materials	14

13. Tunability (%. 1.5 V/micron) versus barium content, Ba(1-x), for undoped materials	15
14. Curie temperature versus barium content, Ba(1-x), for undoped materials	15
15. Dielectric constant versus barium content, Ba(1-x), for materials doped with 2.5 wt% BaLiF ₃	16
16. Tunability (%. 1.5 V/micron) versus barium content, Ba(1-x), for materials doped with 2.5 wt% BaLiF ₃	16
17. Curie temperature versus barium content, Ba(1-x), for materials doped with 2.5 wt% BaLiF ₃	17
18. Barium content, Ba(1-x), and dielectric constant versus grain size for undoped materials	18
19. Barium content, Ba(1-x), versus grain size for undoped materials and materials doped with 1.0 wt% zirconia	18

Tables

1. Sample descriptions of doped BSTO (Ba=0.75) and BaTiO ₃	2
2. Densities and porosity of doped BSTO (Ba=0.75) and doped BaTiO ₃	3
3. Electronic properties of doped BSTO (Ba=0.75) measured at 1 KHz	7
4. Electronic properties of doped BTO measured at 1 KHz	10

Accession For	
NTIS GRA&I	<input checked="" type="checkbox"/>
DTIC TAB	<input type="checkbox"/>
Unannounced	<input type="checkbox"/>
Justification	
By _____	
Distribution/	
Availability Codes	
Dist.	Avail and/or Special
A-1	

Introduction

Phased array antennas can steer the transmitted or received signals either linearly or in two dimensions without mechanical oscillation. These antennas are currently constructed using ferrite phase shifting elements. Due to the type of circuit requirements necessary to operate these antennas, they are costly, large, and heavy; therefore, their use has been limited primarily to strategically dependent military applications. In order to make these devices available for many other commercial and military uses, the basic concept of the antenna must be improved. If ferroelectric material could be used instead of ferrites, phased array antennas would be totally revolutionized.

The concept of using ferroelectric materials for phased array radar systems is not new. However, due to new and sophisticated device fabrication and testing, as well as to the advent of new improvements in electro-ceramic formulations and ceramic processing, the use of these materials seems more realistic than ever.

A ceramic barium strontium titanate (BSTO), $\text{Ba}_{1-x}\text{Sr}_x\text{TiO}_3$, electro-optic phase shifter using a planar microstrip construction has been demonstrated (1). In order to meet the required performance specifications for maximum phase shifting ability, the electronic properties in the low frequency (KHz) and microwave regions (GHz) must be optimized. As part of this optimization process various dopants have been added to the material and their effects on the electronic properties have been studied. The relationships between the effect of these dopants on the dielectric constants, tunability, grain size, Curie temperature and, in some cases, strontium content have been investigated and will be discussed in this report. This report will outline some of the initial findings and compare the results found for some of the dopants to the results obtained in doped BaTiO_3 (BTO).

Experimental

Ceramic Processing

Table 1 contains the additives, sample numbers, calcining, and sintering temperatures for the specimens examined in this investigation. Various oxide and fluoride additives were mixed with BaTiO_3 (Ferro Corp. #219-6) and SrTiO_3 (Ferro Corp. #218) in a formulation for additive testing of $\text{Ba}_{0.75}\text{Sr}_{0.25}\text{TiO}_3$. The mixture was ball milled in ethanol using alumina grinding media for about 24 hours and subsequently air dried. The powder is then calcined at the temperatures given in Table 1. The calcined material was then made into a slurry with ethanol and ball milled with alumina grinding media for 24 hours. At this time, 3 wt% organic binder from Rohm and Haas Company, product Rhoplex B-60A which is an aqueous emulsion of acrylic polymer, was added to improve green body strength and permit sample fabrication. The mixture was then ball milled for another four to five hours and air dried. The powder was cold uniaxially pressed at a pressure of approximately 7000 psi. The pellets were sintered at the temperatures given in Table 1 for an average soak time of about two hours. Table 2 gives the final geometrical densities, % theoretical density, % porosity (open) and % liquid absorption (ethanol) for the specimens listed in Table 1. The % porosity and the % liquid absorption were determined from immersion density methods, using specimens which were placed in a vacuum and then saturated with ethanol; the % porosity was determined from the dry weight, the saturated weight, and the suspended (in ethanol) saturated weights.

Table 1. Sample descriptions of doped BSTO (Ba=0.75) and BaTiO₃

Sample #	Additive	Calcining temp. (°C)	Sintering temp. (°C)
BSTO			
A30	1 wt% ZrO ₂	1100	1325
A31	1 wt% ZrO ₂ , 1 wt% BaLiF ₃	700	1335
A32	5 m% Bi ₂ (SnO ₃) ₃	1100	1350
A33	5 m% Bi ₂ (SnO ₃) ₃ , 1 wt% BaLiF ₃	700	1335
A35	1.8 wt% CaSnO ₃	1100	1325
A36	2 wt% CaTiO ₃	1100	1325
A37	2 m% NiSnO ₃	1100	1350
A38	2.5 wt% BaLiF ₃ , CaO, MnO ₂	700	1325
A39	1 wt% Al ₂ O ₃	1100	1335
A40	30 wt% Al ₂ O ₃	1100	1335
A68	Undoped	1100	1335
BaTiO₃			
A58	1 wt% ZrO ₂ , 1 wt% BaLiF ₃	700	1335
A59	5 m% Bi ₂ (SnO ₃) ₃	1100	1335
A60	30 wt% Al ₂ O ₃	1100	1335
A61	1 wt% Al ₂ O ₃	1100	1335
A62	2.5 wt% BaLiF ₃ , CaO, MnO ₂	700	1350
A63	2 m% NiSnO ₃	1100	1350
A64	2 wt% CaTiO ₃	1100	1325
A65	6 wt% CaTiO ₃ , 4 wt% CaSnO ₃	1100	1350
A66	2 m% CaSnO ₃	1100	1325
A67	5 m% Bi ₂ (SnO ₃) ₃ , 1 wt% BaLiF ₃	700	1335
A69	Undoped	1100	1335

Table 2. Densities and porosity of doped BSTO (Ba=0.75) and doped BaTiO₃

Sample #	Density (g/cm ³)	% Theoretical density	% Porosity	% Liquid absorption
BSTO				
A30	5.44	96	2.31	0.34
A31	5.13	91	5.58	0.84
A32	5.22	92	2.25	0.33
A33	5.19	91	2.54	0.36
A35	5.32	94	1.01	0.15
A36	5.14	91	9.15	1.45
A37	5.20	92	2.41	0.35
A38	5.11	90	2.48	0.36
A39	5.20	92	2.36	0.36
A40	3.97	—	6.76	1.44
A68	5.54	97	0.62	0.08
BaTiO₃				
A58	5.49	94	5.95	0.88
A59	5.79	99	3.95	0.54
A60	3.40	—	17.82	4.02
A61	5.22	90	4.96	0.80
A62	5.13	88	20.12	3.35
A63	5.97	100	3.69	0.55
A64	5.32	91	6.45	0.97
A65	5.70	97	5.26	0.87
A66	5.80	99	6.00	0.87
A67	5.62	96	7.22	1.03

Electronic Measurements

Before discussing the electronic properties of the materials, some definitions are required. The dielectric constant of a given material can be related to the amount of energy storage by measuring the capacitance (F) of the material, where $\epsilon = C(F) \times d / \epsilon_0 A$, d = thickness, A = area, and $\epsilon_0 = 8.8542 \times 10^{-12}$ F/m. In general, for any given material the dielectric constant $\epsilon = \epsilon' - i\epsilon''$. The loss tangent ($\tan \delta$) of the material is related to the energy dissipated and is given by the ratio of the imaginary part of the dielectric constant ϵ'' divided by the real part ϵ' . The Curie temperatures, dielectric constants, ϵ' , and % tunability was determined at the ARL-Microwave and Photonics Branch Electronic Power Sources Directorate. The tunability of a material is defined as:

$$\% \text{ tunability} = (\epsilon(0) - \epsilon(V_{\text{app}})) / (\epsilon(0)). \quad (1)$$

The block diagram of the experimental apparatus for measuring the tunability, dielectric constants, Curie temperature, and hysteresis is shown in Figure 1. The sample is encapsulated in a dry box and is heated and cooled with a thermoelectric cooler (TEC). The TEC has two wires connected to the computer controlled by a double throw switch which changes the polarity of the voltage applied to the TEC. The temperature is held within $\pm 0.05^{\circ}\text{C}$. The device under test (DUT) is painted on both sides with silver epoxy and mounted to the brass plate holder with epoxy. A wire is fixed to the top of the specimen and held in place with a TeflonTM plate, and tightened with two tension screws, as shown in Figure 2. The fixture is placed in an oven at 150°C for one hour to anneal the silver epoxy; then, the specimen is placed into a dry box and the test is run. The data includes standard deviation at each point. The tunability measurements were taken with an applied electric field which ranged from 0 V/micron to 1.5 V/micron. All of the electronic properties reported here were measured at a frequency of 1 KHz.

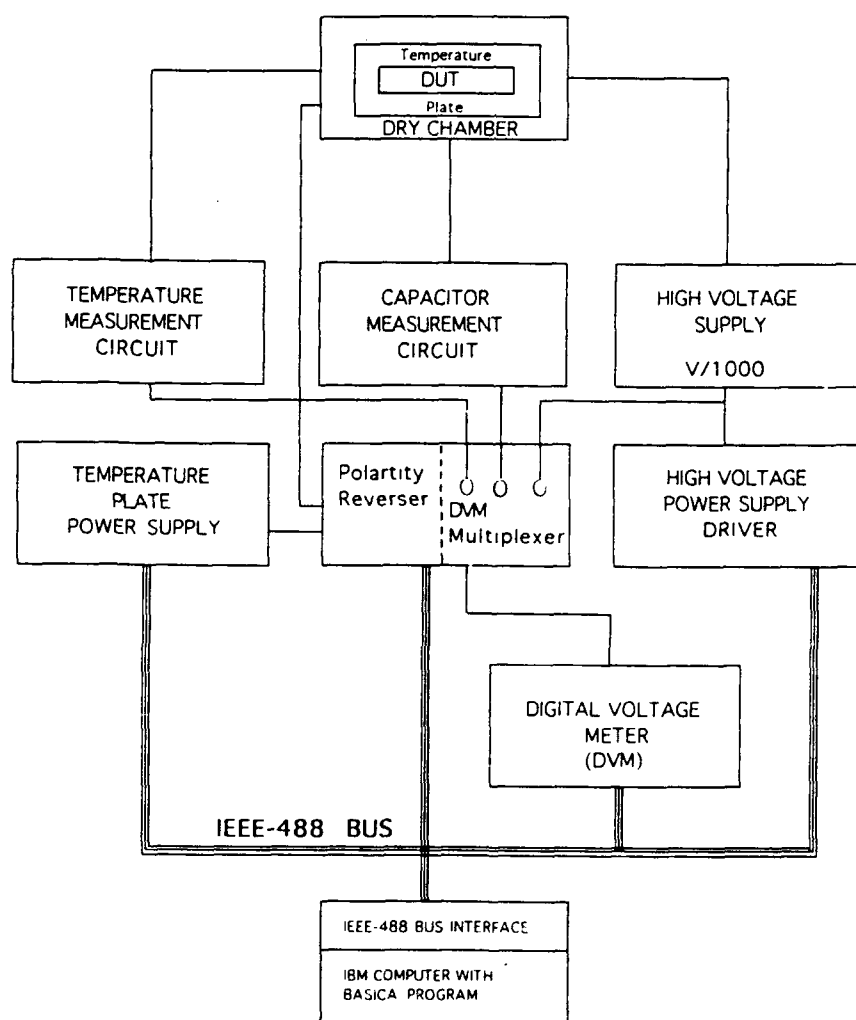


Figure 1. Block diagram of ARL-EPD electronic test equipment.

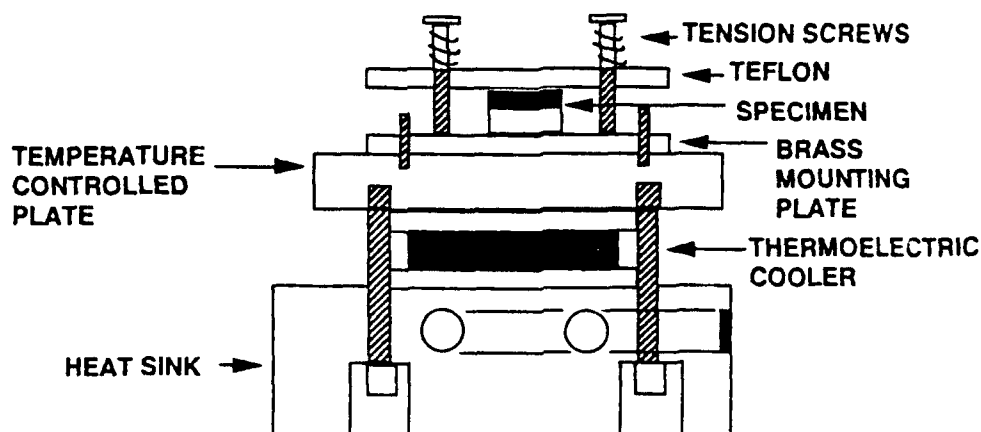


Figure 2. Specimen holder and heating apparatus for electronic test system

Results and Discussion

The inverse of the dielectric constant versus temperature for samples A68 and A30 are shown in Figures 3(a) and 3(b). The degree of homogeneity in the materials can be determined from how well the data obeys the Curie-Weiss law, where:

$$1/\epsilon = 1/\epsilon_0 ((T-T_c)/(T + 2T_c)), \quad (2)$$

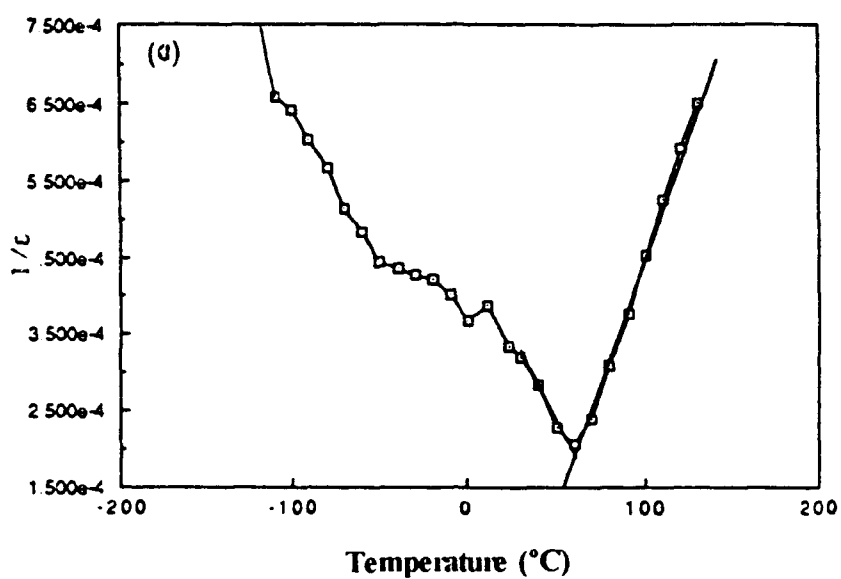
T_c = Curie temperature, $\epsilon_0 = 8.8542 \times 10^{-12}$ F/m.

Using the data shown in Figure 3, the relationship described by Equation 2 is followed until 2°C of the Curie temperature (40°C). This indicates that the sample is highly uniform and that the dielectric properties of the bulk are representative of the entire specimen.

Dopants in BSTO (Ba=0.75)

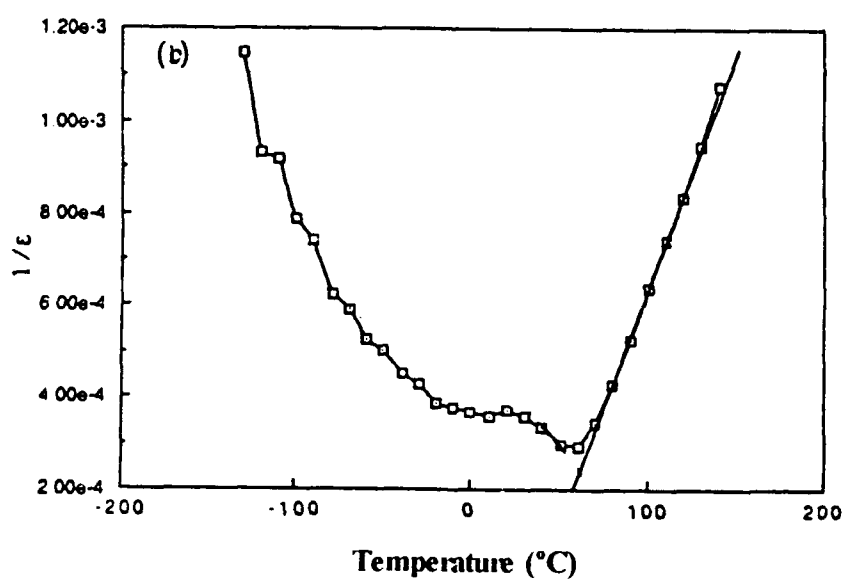
A summary of the electronic properties of the doped BSTO (Ba=0.75) specimens is given in Table 3. The specimens were measured at 1 KHz and the electric field was increased to $1.5 \text{ V}/\mu\text{m}$. Dopants that were studied in this investigation either substitute for the Ba site or the Ti site in the material. Generally, the dopants, which are compounds, will have constituents that will predominantly substitute into these lattice positions. The effects of these substitutions are: if substituted into the Ba site to shift the Curie temperature, or if substituted into the Ti site to suppress the Curie temperature. Compound dopants ultimately occupy intergranular positions and do not combine totally into the lattice positions. Therefore, studying the electronic behavior can indicate the subtle effect of the dopants on the crystal structure of the materials even if the lattice parameters and X-ray diffraction patterns are not affected. To clarify the differences between the effect of the dopant and that of Sr in the ceramics, identical dopants have been added to barium titanate.

BSTO (Ba=0.75) undoped



(a)

BSTO (Ba=0.75) & 1wt% ZrO2



(b)

Figure 3 Curie-Weiss relationship $1/\epsilon$ versus temperature for: (a) an undoped specimen, and (b) a specimen doped with 2 wt% zirconia.

Table 2 Electronic properties of doped BSTO (Ba=0.75) measured at 1 KHz

Sample #	Dielectric constant	Curie temperature (°C)	Tunability (%)	Hysteresis (%)
A30	1630	60	28.0	2.0
A31	1388	55	27.0	2.0
A32	1193	54	23.0	0.2
A33	549	-60	1.5	0.2
A35	675	55	17.0	—
A36	474	60	17.0	2.0
A38	532	40	23.0	0.3
A39	930	50	28.0	0.6
A40	25	—	4.0	0.1
A68	1150	60	32.0	5.0

For a clearer understanding of the trends found in the results, some of the data will be presented in a graphic format, as shown in Figures 4 and 5. It is obvious from these figures (Figure 4 shows the dielectric constant versus tunability and Figure 5 shows the Curie temperature versus tunability) that the tunability increases with increasing dielectric constant and also with increasing Curie temperature. This is a direct consequence of the fact that the tunability is greatest at the peak of the Curie temperature and is also high at temperatures below the Curie point where the material is in the *ferroelectric* region. At temperatures far above the Curie temperature (in the *paraelectric* region) for a particular composition the tunability drops off rapidly. Likewise, the dielectric loss of any given material is decreased when the material is measured in its paraelectric region or, in other words, when the Curie temperature is decreased. This was observed for sample A30 (1 wt% zirconia) which had a loss tangent of 0.36 at 10 GHz (Curie temperature of 60°C, dielectric constant = 1630) as compared to sample A31 which was doped with 1 wt% zirconia and 1 wt% BaLiF₃ (Curie temperature of 55°C, dielectric constant = 1388) and has a loss tangent of 0.15. As seen above, the loss tangent seems to decrease with dielectric constant. A30 and A31 can be compared to A39 (doped with 30 wt% alumina) which at 39 GHz has a dielectric constant of 45.8 and a loss tangent of 0.054. The loss tangent is definitely less for the lower dielectrics. It should be noted that compositions which had Curie temperatures below room temperature had a tunability of less than 10%. The % hysteresis is not directly related to changes in the dielectric properties. However, in the paraelectric region the hysteresis is thought to be due to aging under bias.

The grain size of the material is related to the electronic properties, as can be seen in Figure 6. As the grain size decreases, the dielectric constant increases in these materials and the increase reaches a maximum at grain sizes of around 10 microns. This behavior has been noted previously and has been attributed to an increase in the domain width and increase in internal stress below a critical grain size (2). Figure 7 shows the tunability and the Curie temperature versus grain size. As expected, below a critical grain size of about 1 micron both the tunability and Curie temperature decrease drastically.

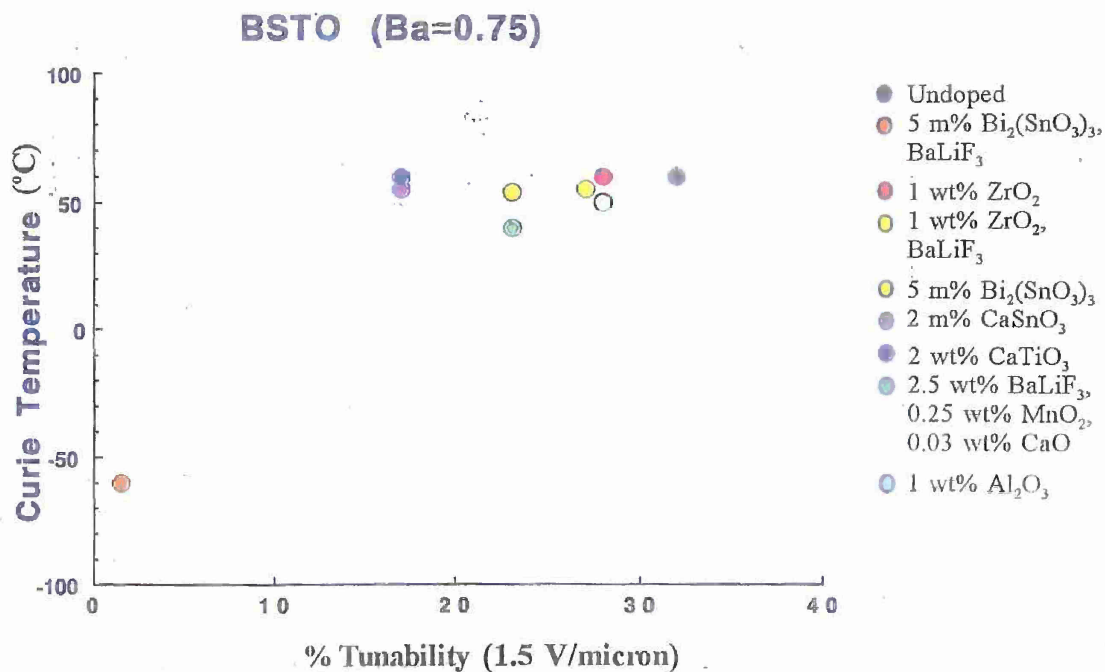


Figure 4. Dielectric constant versus tunability (1.5 V/micron) for doped BSTO (Ba=0.75).

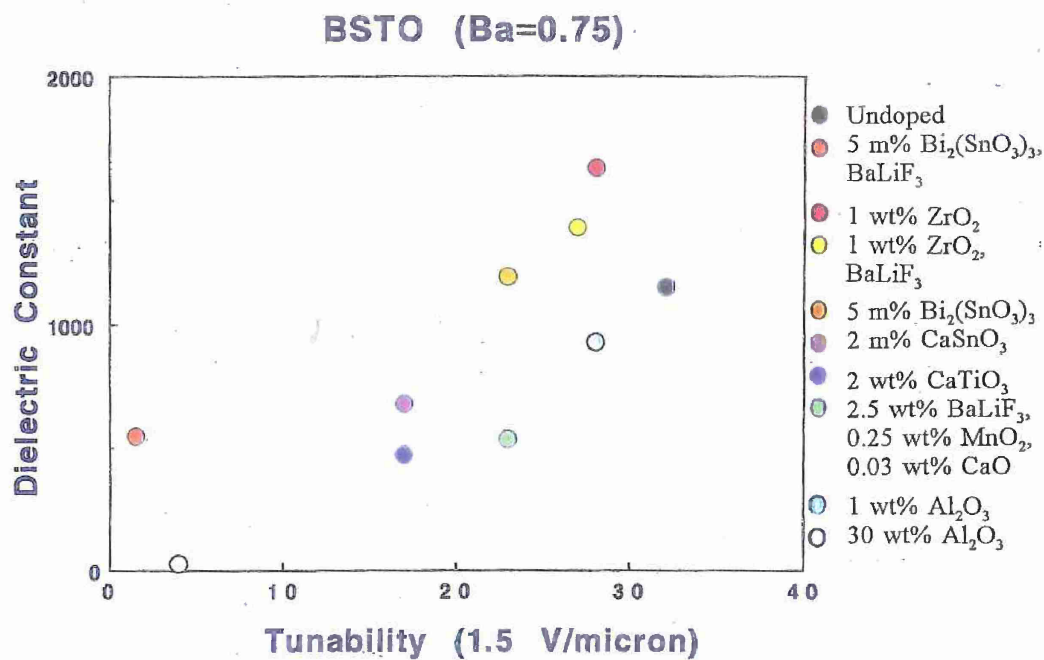


Figure 5. Curie temperature (°C) versus % tunability (1.5 V/micron) for doped BSTO (Ba=0.75).

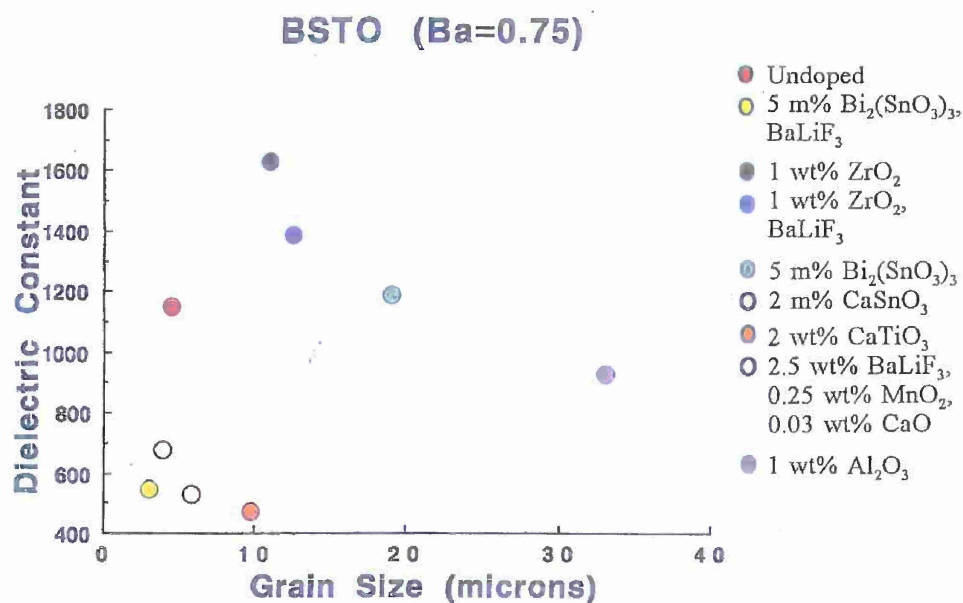


Figure 6. Dielectric constant versus grain size for doped BSTO (Ba=0.75).

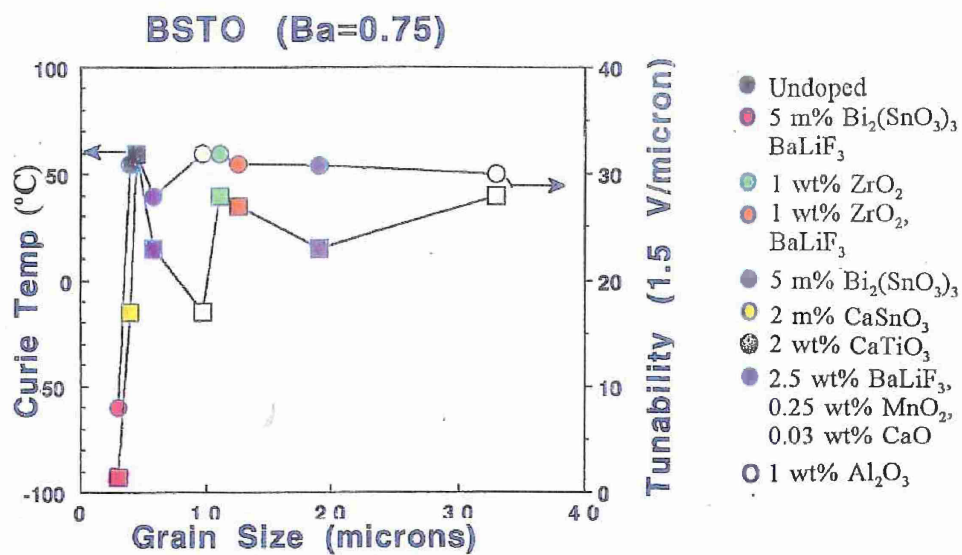


Figure 7. Curie temperature and tunability (1.5 V/micron) versus grain size for doped BSTO (Ba=0.75).

Dopants in BTO

The results of the electronic properties of BTO doped with the identical dopants of the BSTO samples are shown in Table 4. As shown in Figures 8 and 9, similar results are shown for the dopants when added to BTO. As expected, the tunability, in general, is less than the BSTO (Ba=0.75) samples; this is because the Curie temperature of undoped barium titanate is very much above room temperature (120°C). The primary reason strontium is used is the fact that controlling the Curie temperature is the most effective method for controlling tunability. As obtained for the doped BSTO (Ba=0.75) materials, the tunability decreases when any dopant is added to pure barium titanate. Also, similar to BSTO, the doped BTO samples with the lowest tunabilities (samples A59 and A67) have the lowest Curie temperatures which are below room temperature. This, again, leads to the conclusion that when operating these ferroelectric materials in the paraelectric region the tunability is decreased. However, as shown in Table 4, and as stated before, the loss is also decreased (these losses are approximate values). However, the dielectric constant does not increase with an increase in tunability and is not clearly related to the tunability as in the case of BSTO. This is probably because of the differences in the Curie temperature in the case of BSTO as compared to BTO. In the case of BSTO (Ba=0.75), the peak of the dielectric constant (40°C) is near to the operating (room) temperature; therefore, small variations in the position on this curve make a large difference in the value obtained for the dielectric constant as well as in the tunability. On the other hand, for BTO (Curie temperature = 120°C) at room temperature, the dielectric constant curve is fairly flat. Small changes in the dielectric cannot greatly affect the tunability. Also, the magnitude of the change in the dielectric is not as great as that experienced with the BSTO samples.

Table 4. Electronic properties of doped BTO measured at 1 KHz

Sample #	Dielectric constant	Curie temperature (°C)	Tunability (%)	Tan δ
A58	814	110	17.0	0.100
A59	575	-70	0.8	0.010
A60	14	40	1.0	0.010
A61	880	130	10.0	0.100
A62	1267	100	13.0	0.010
A63	1617	130	8.0	0.010
A64	695	135	3.0	0.010
A65	97	90	5.0	0.010
A67	410	-50	0.4	0.010
A69	952	120	22.0	0.100

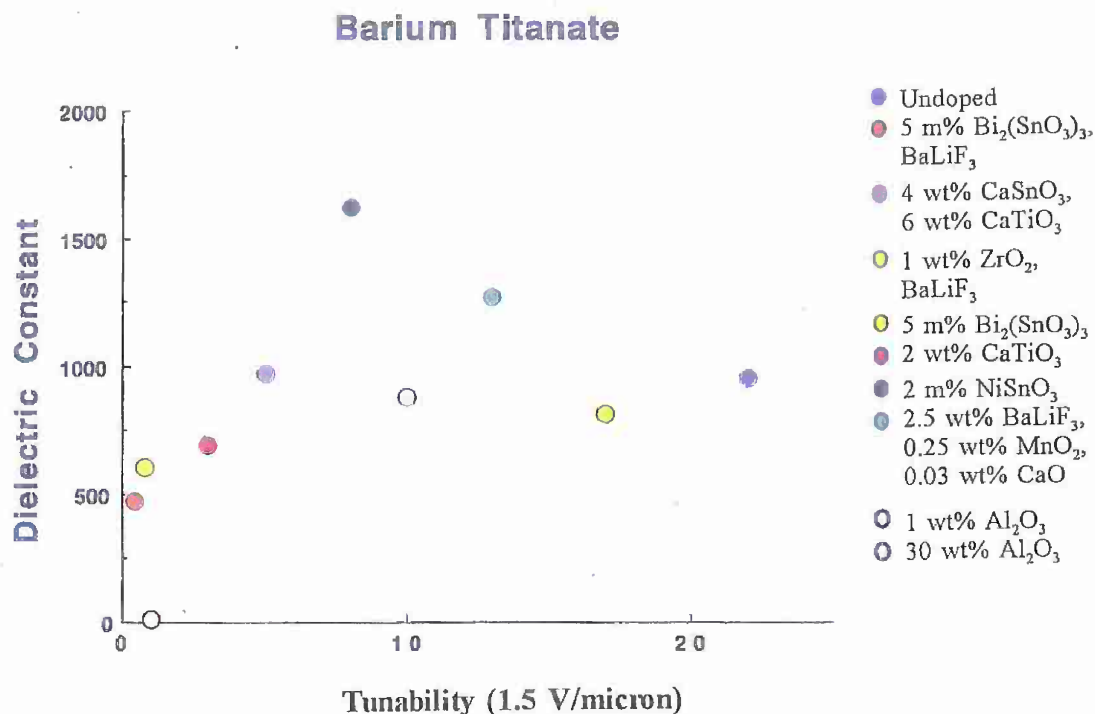


Figure 8. Dielectric constant versus tunability (1.5 V/micron) for doped BTO.

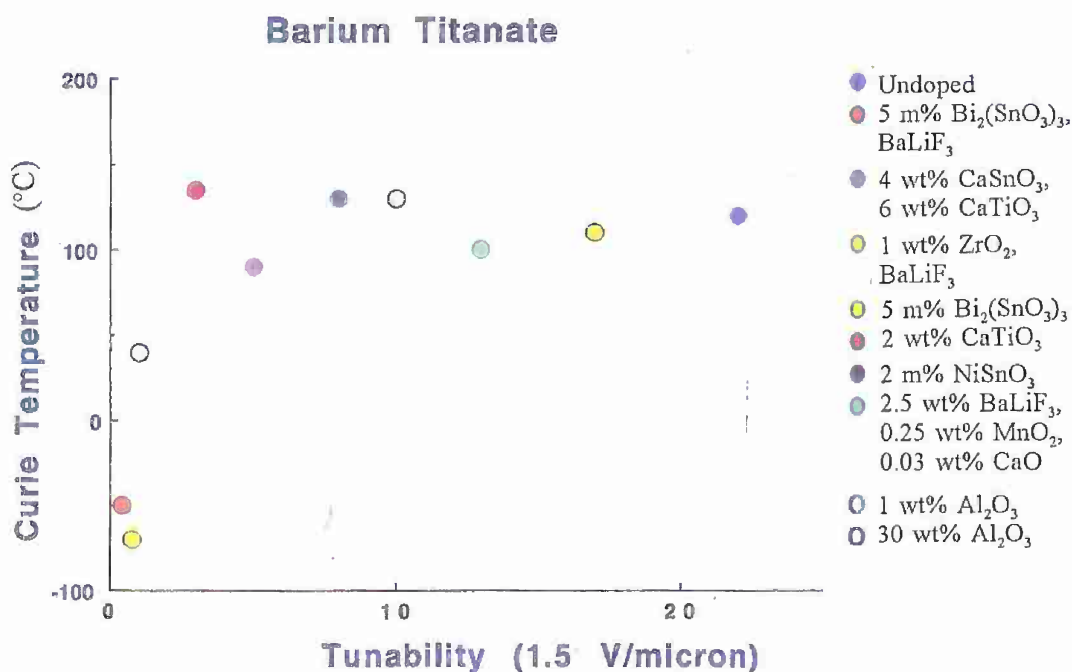


Figure 9. Curie temperature (°C) versus % tunability (1.5 V/micron) for doped BTO.

The grain size versus dielectric constant of the doped BTO samples are shown in Figure 10. As seen in the case of the doped BSTO samples, the dielectric increases with the decrease in grain size until about 1 μm . This result has been reported previously and was attributed to the decrease in domain width and the increase in internal stress (2). The grain size below, which the dielectric begins to decrease, is less in the case of BTO as compared to BSTO. As shown in Figure 11, the tunability and

THIS
PAGE
IS
MISSING
IN
ORIGINAL
DOCUMENT

Curie temperature decrease rapidly below a grain size of 1 micron, which was the case for BSTO. This produced investigation of the grain size and the electronic properties as a function of Ba(1-x) content in the material which will be discussed in the following section.

Barium Titanate

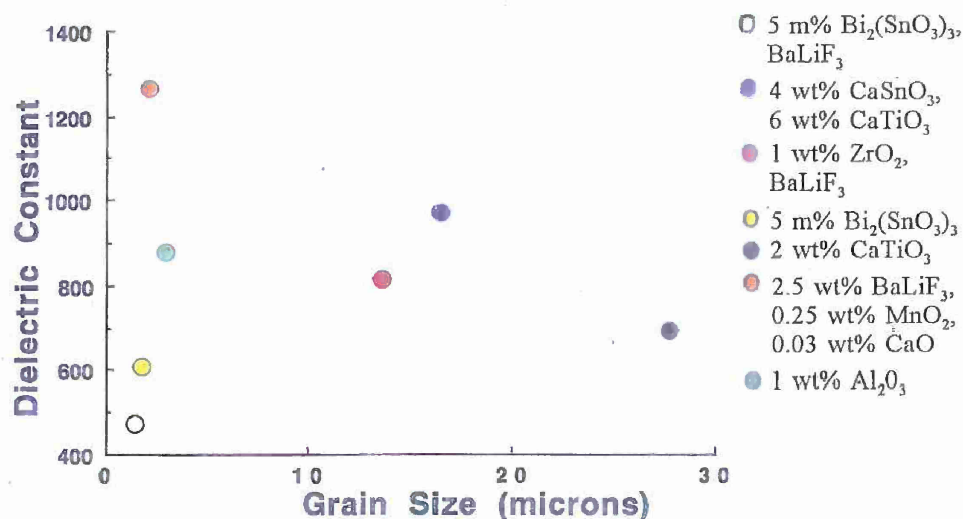


Figure 10. Dielectric constant versus grain size for doped BTO.

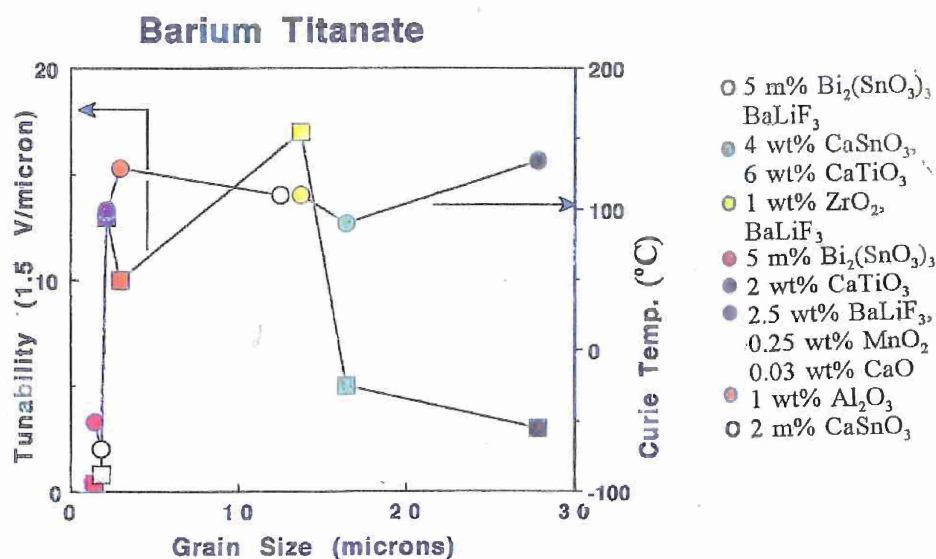


Figure 11. Curie temperature and tunability (1.5 V/micron) versus grain size for doped BTO.

Variation of Ba(1-x) Content in Undoped and Doped BSTO

As shown in Figure 12, the dielectric constant is a maximum at barium content between $1-x = 0.65$ to 0.70 . This is because these compositions have Curie temperatures which are at room temperature and, therefore, represent peak dielectric constants for the material. Figure 13 shows the tunability versus Ba(1-x) content. The tunability is also a maximum for compositions in the range from $1-x = 0.65$ to 0.75 . Again, this is due to the temperature at which the peak dielectric constant occurs which is, for these compositions, around room temperature. Since the tunability is essentially the derivative with respect to voltage of the dielectric constant curve, the maximum tunability should occur at the steepest point of the curve which is at room temperature for those compositions. The Curie temperature versus composition (Ba(1-x)) is shown in Figure 14. As displayed in Figure 14, the relationship is linear. This linearity and controllability is due to the fact that the addition of strontium changes the phase of the material from tetragonal at room temperature for barium titanate to cubic at room temperature for BSTO, with a linear decrease in the lattice constant as the strontium content is increased. Since the addition of strontium offers this very linear and controlled modification of the Curie temperature in barium titanate, it has been a widely used additive and is commonly used in the capacitor industry.

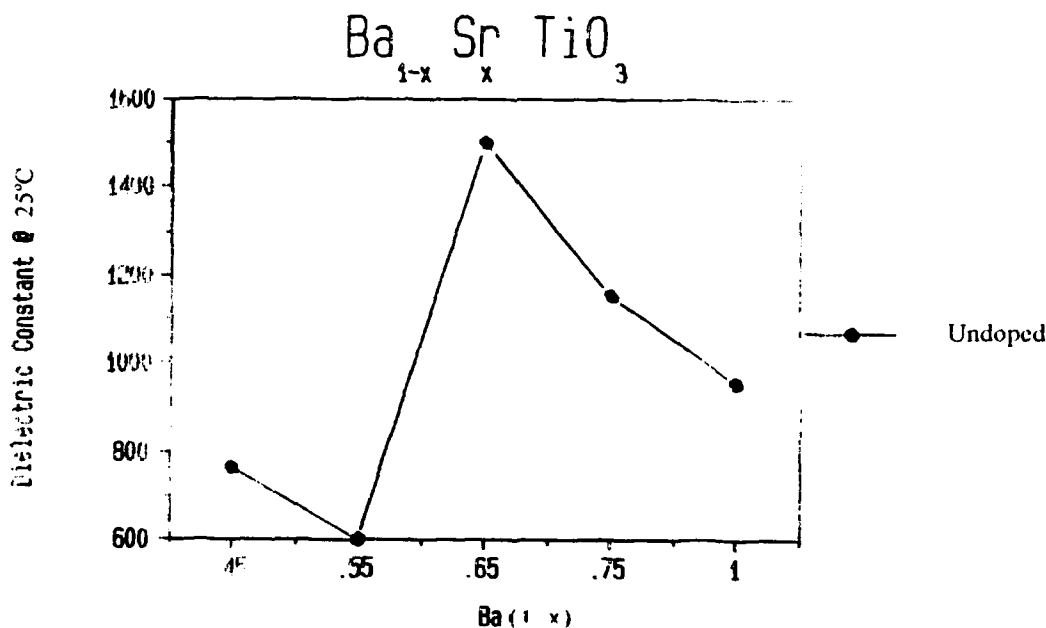


Figure 12. Dielectric constant versus barium content, (Ba(1-x)), for undoped materials.

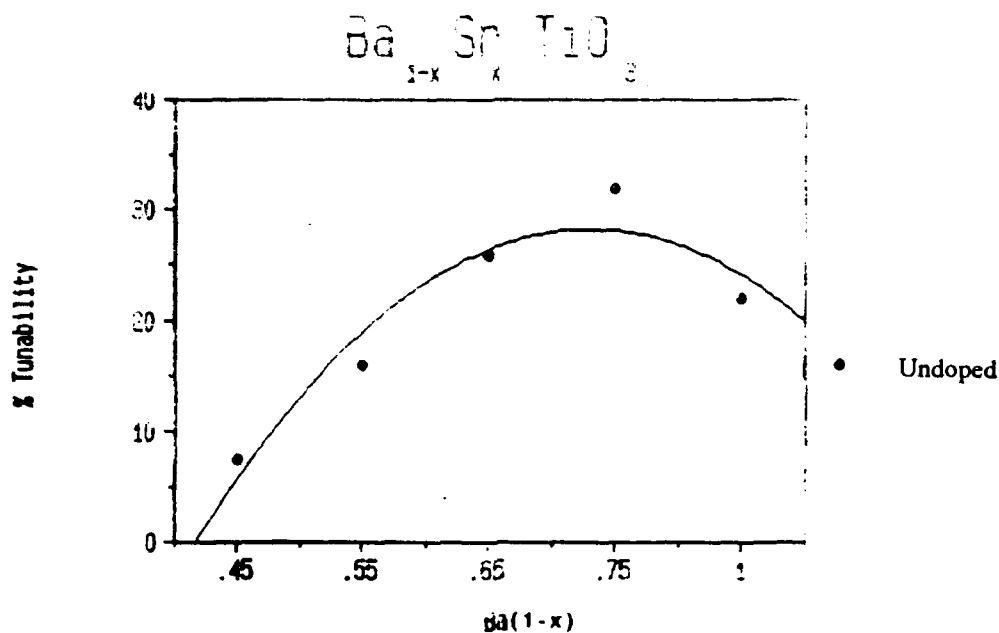


Figure 13. Tunability (% 1.5 V/micron) versus barium content, Ba(1-x), for undoped materials.

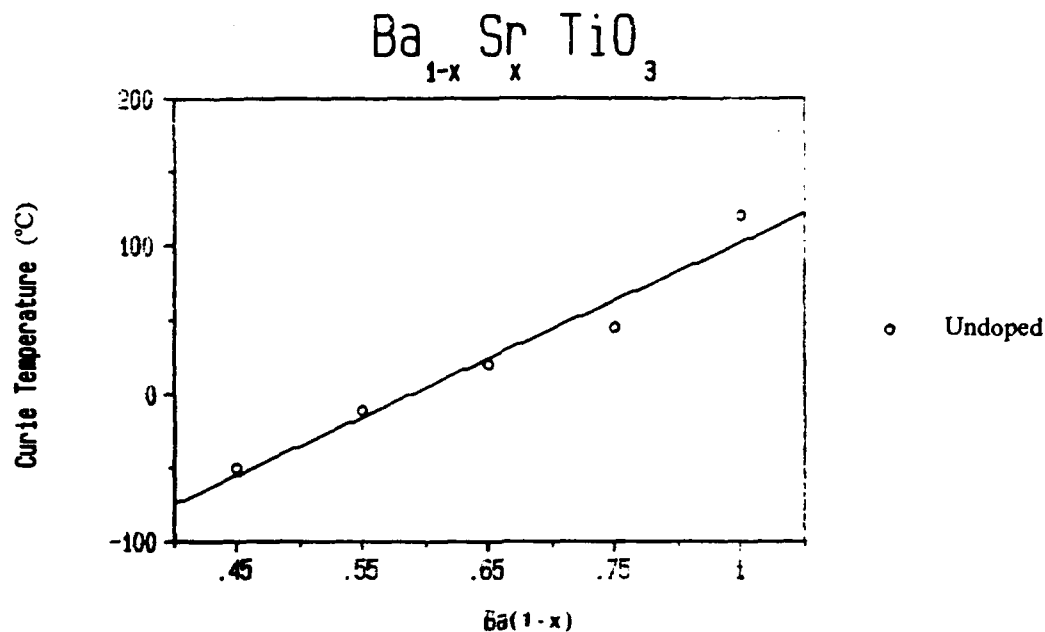


Figure 14. Curie temperature versus barium content, Ba(1-x), for undoped materials.

Figures 15, 16, and 17 show the relationship between the dielectric constant, tunability, Curie temperature, and barium content for specimens doped with BaLiF₃. The relationships of the electronic properties (dielectric, constant, Curie temperature, and tunability) versus Sr composition are unchanged when other dopants such as BaLiF₃ is added to the material. The electronic properties versus Ba(1-x) content are also unchanged for ZrO₂ samples. This indicates that these other dopants, at the levels incorporated, have little effect on the lattice constants and crystal structure of the material.

This was indeed found from the X-ray diffraction data which did not show any change in the lattice constants (compared to the undoped materials with the same Sr content). The dopants, however, do decrease the tunability and, in the case of the fluoride dopants, the dielectric constant is decreased. Zirconia at this level of substitution does not decrease the dielectric constant.

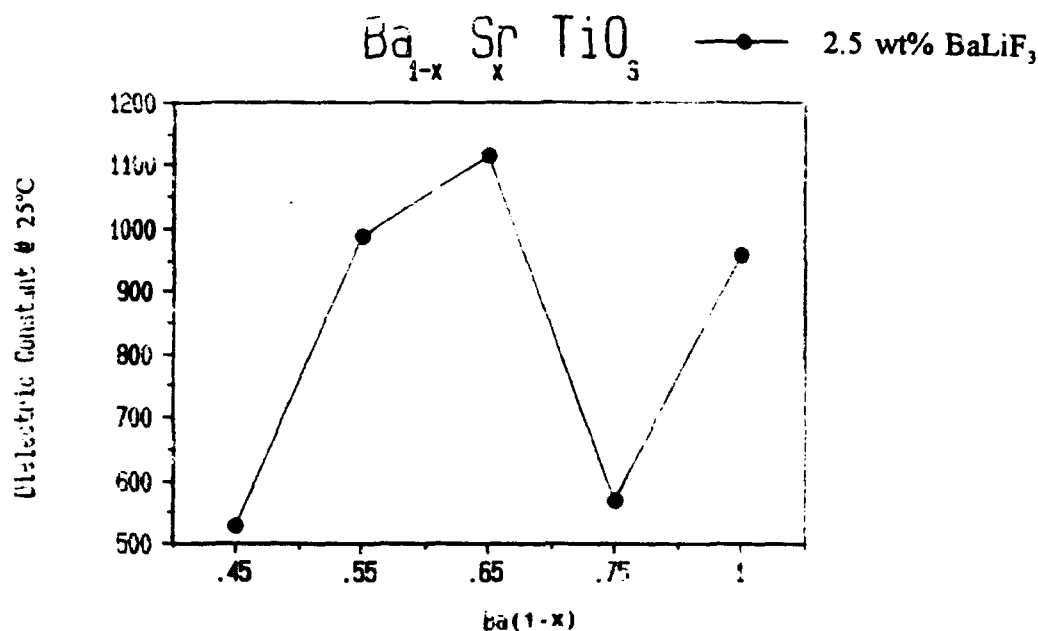


Figure 15. Dielectric constant versus barium content, Ba(1-x), for materials doped with 2.5 wt% BaLiF₃.

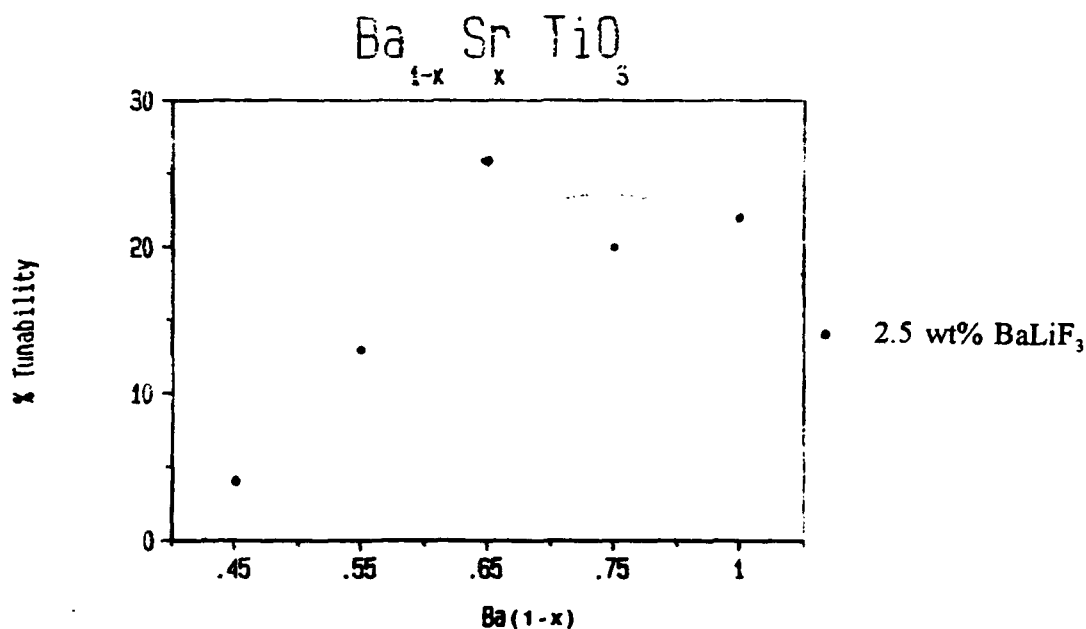


Figure 16. Tunability (% 1.5 V/micron) versus barium content, Ba(1-x), for materials doped with 2.5 wt% BaLiF₃.

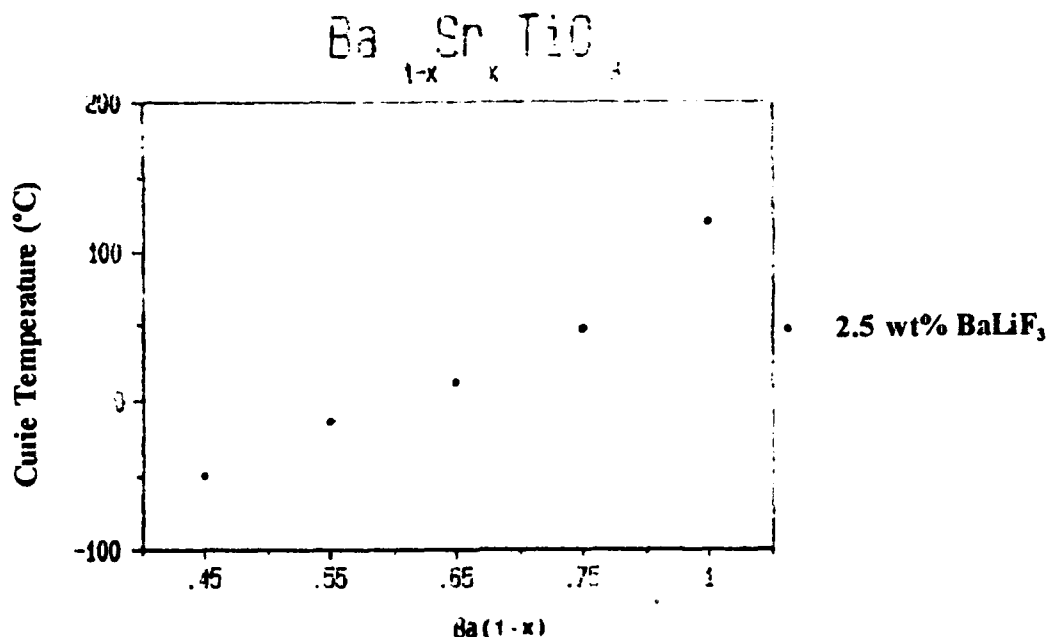


Figure 17. Curie temperature versus barium content, $Ba(1-x)$, for materials doped with 2.5 wt% BaLiF₃.

Figure 18 shows the $Ba(1-x)$ content and dielectric constant versus grain size for undoped specimens. As seen in the figure, the grain size increases with the increase in $Ba(1-x)$ content, which is as expected. However, the dielectric constant increases with the decrease in grain size, which indicates a maximum dielectric constant at a grain size of about 10 microns (composition of about $Ba(1-x) = 0.65$). Then, the dielectric constant decreases with further decrease in grain size below 10 microns. The decrease in dielectric constant is probably due to the shift in Curie temperature, as well as grain size effects.

Figure 19 shows the grain size versus $Ba(1-x)$ content for doped BSTO with 1 wt% ZrO₂ as compared to the undoped specimens. It is obvious that the addition of zirconia decreases the grain size. The data does indicate a slight decrease in the dielectric constant for compositions where the grain size is also the most dramatically affected; i.e., for barium content = 1.00, 0.75, and 0.65. However, specimens with varying barium content doped with zirconia showed identical trends in the dielectric constant and other electronic properties versus barium content as the undoped and the specimens doped with BaLiF₃. This is probably because zirconia does effect the Curie temperature as does the strontium titanate; therefore, the change in the dielectric constant with the change in the barium content is the dominant effect at this level of zirconia substitution. The substitution of zirconia does broaden the Curie temperature and decreases the dielectric constant for compositions which are in the ferroelectric region, and this broadening effects room temperature dielectric constant data.

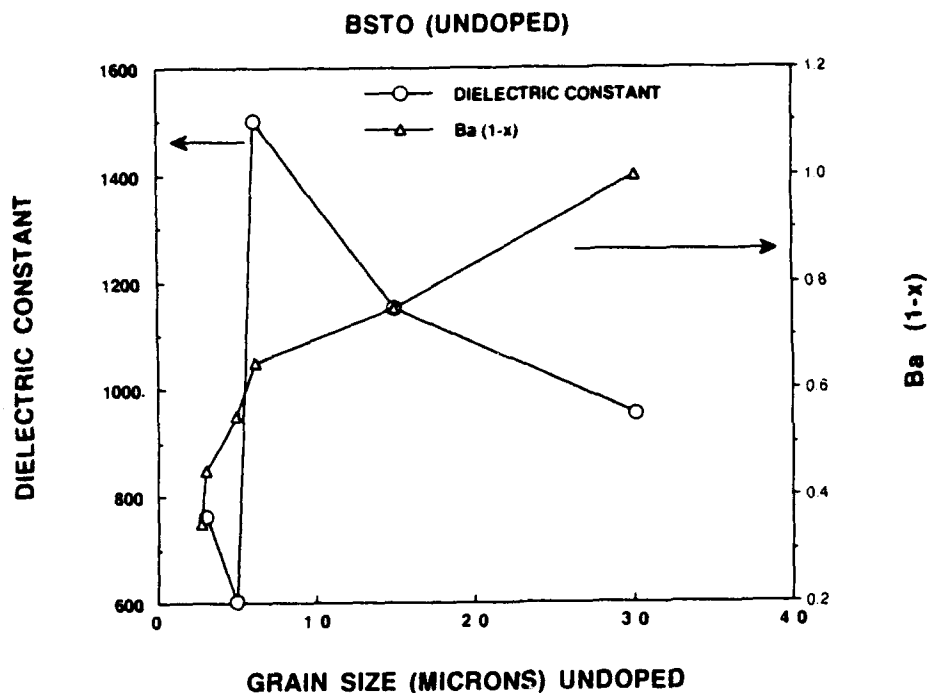


Figure 18. Barium content, $Ba(1-x)$, and dielectric constant versus grain size for undoped materials.

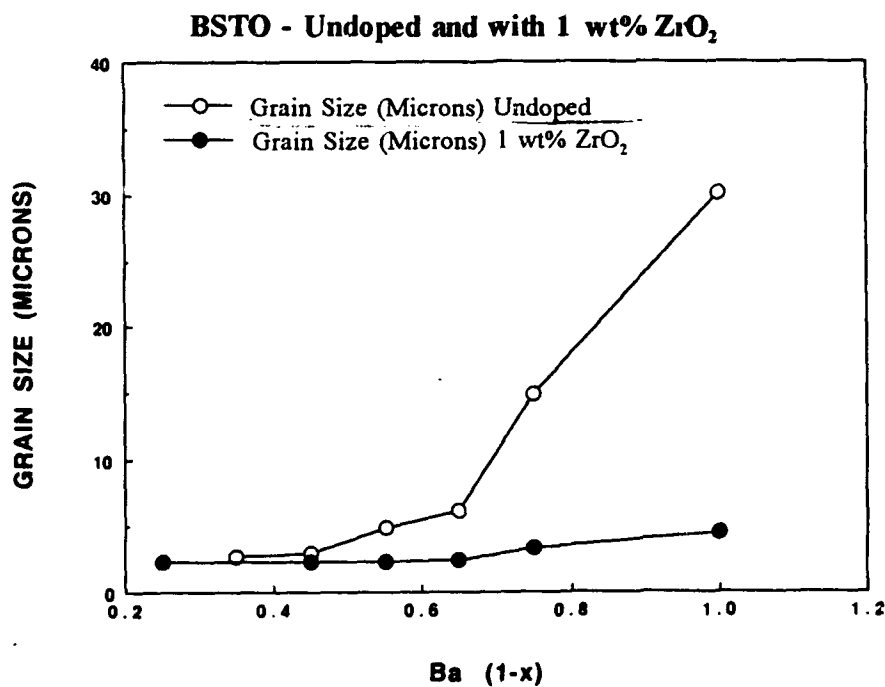


Figure 19. Barium content, $Ba(1-x)$, versus grain size for undoped materials and materials doped with 1.0 wt% zirconia.

Conclusions

For dopant modifications BSTO ($\text{Ba}(1-x) = 0.75$) as studied in this investigation, it was found that the tunability increases with an increase in the dielectric constant and with an increase in Curie temperature. The tunability, however, is the greatest in the undoped material. The loss tangent (10 GHz) was also found to increase with an increase in the Curie temperature. This is because the loss tangent is the greatest when the material is in the ferroelectric phase; therefore, it is the greatest for materials which have Curie temperatures at and above room temperature.

BTO with the same additives as used in the above mentioned portion of this investigation shows similar electronic behavior. The tunability obtained for these specimens even in the undoped specimen is less than in the BSTO (0.75) samples. Also, the dopants again reduce the tunability as compared to the undoped BTO specimen. The dielectric constant is not as clearly related to the tunability as in the BSTO materials. This is because the Curie temperature of almost all of these samples are far above room temperature.

Variation of the barium content shows that the maximum tunability and dielectric constant occur at a barium content $\text{Ba}(1-x) = 0.65$. This is because this composition has a Curie temperature at room temperature. Therefore, the peak dielectric constant and the room temperature dielectric constant coincide. Also, the Curie temperature increases linearly with an increase in barium content. BaLiF_3 and ZrO_2 at the levels incorporated in this study do not change the relationships described above.

The grain size is related to the electronic properties. For the doped BSTO (0.75) specimens, the dielectric constant increases with a decrease in grain size; then, beyond a critical grain size of 10 microns the dielectric constant decreases. Similar behavior was found in the doped BTO specimens. The grain size of the specimens decreases with the decrease in barium content and also when zirconia is added. The zirconia doped materials show less of a dependence on barium content. In order to further clarify relationships between microstructures and electronic properties, various amounts of the same dopant will be added to a single composition of BSTO. However, it is clear that the grain size plays an important role in controlling the electronic properties of the BSTO, and the grain size seems to effect all of the electronic properties simultaneously.

Acknowledgments

The authors would like to thank the engineers of Transelco Division of Ferro Corporation in particular Jim Henry and Jim Wilson for their kind donations of advice and materials.

References

1. BABBITT, R. W., KOSCICA, T. E., and DRACH, W. E. Microwave Journal, v 35, 1992, p. 63.
2. ARLT, G., HENNINGS, D., and deWITH, G. J. Appl. Phys., v. 58, 1985, p. 1619.

DISTRIBUTION LIST

No. of Copies	To
1	Office of the Under Secretary of Defense for Research and Engineering, The Pentagon, Washington, DC 20301
	Director, U.S. Army Research Laboratory, 2800 Powder Mill Road, Adelphi, MD 20783-1197
1	ATTN: AMSRL-OP-CI-AD, Technical Publishing Branch
1	AMSRL-OP-CI-AD, Records Management Administrator
	Commander, Defense Technical Information Center, Cameron Station, Building 5, 5010 Duke Street, Alexandria, VA 23304-6145
2	ATTN: DTIC-FDAC
1	MIA/CINDAS, Purdue University, 2595 Yeager Road, West Lafayette, IN 47905
	Commander, Army Research Office, P.O. Box 12211, Research Triangle Park, NC 27709-2211
1	ATTN: Information Processing Office
	Commander, U.S. Army Materiel Command, 5001 Eisenhower Avenue, Alexandria, VA 22333
1	ATTN: AMCSCI
	Commander, U.S. Army Materiel Systems Analysis Activity, Aberdeen Proving Ground, MD 21005
1	ATTN: AMXSY-MP, H. Cohen
	Commander, U.S. Army Missile Command, Redstone Arsenal, AL 35809
1	ATTN: AMSMI-RD-CS-R/Doc
	Commander, U.S. Army Armament, Munitions and Chemical Command, Dover, NJ 07801
2	ATTN: Technical Library
	Commander, U.S. Army Natick Research, Development and Engineering Center, Natick, MA 01760-5010
1	ATTN: Technical Library
	Commander, U.S. Army Satellite Communications Agency, Fort Monmouth, NJ 07703
1	ATTN: Technical Document Center
	Commander, U.S. Army Tank-Automotive Command, Warren, MI 48397-5000
1	ATTN: AMSTA-ZSK
1	AMSTA-TSL, Technical Library
	Commander, White Sands Missile Range, NM 88002
1	ATTN: STEWS-WS-VT
	President, Airborne, Electronics and Special Warfare Board, Fort Bragg, NC 28307
1	ATTN: Library
	Director, U.S. Army Research Laboratory, Weapons Technology, Aberdeen Proving Ground, MD 21005-5066
1	ATTN: AMSRL-WT

No. of Copies	To
1	Commander, Dugway Proving Ground, UT 84022 ATTN: Technical Library, Technical Information Division
1	Commander, U.S. Army Research Laboratory, 2800 Powder Mill Road, Adelphi, MD 20783 ATTN: AMSRL-SS
1	Director, Benet Weapons Laboratory, LCWSL, USA AMCCOM, Watervliet, NY 12189 ATTN: AMSMC-LCB-TL
1	AMSMC-LCB-R
1	AMSMC-LCB-RM
1	AMSMC-LCB-RP
3	Commander, U.S. Army Foreign Science and Technology Center, 220 7th Street, N.E., Charlottesville, VA 22901-5396 ATTN: AIFRTC, Applied Technologies Branch, Gerald Schlesinger
1	Commander, U.S. Army Aeromedical Research Unit, P.O. Box 577, Fort Rucker, AL 36360 ATTN: Technical Library
1	U.S. Army Aviation Training Library, Fort Rucker, AL 36360 ATTN: Building 5906-5907
1	Commander, U.S. Army Agency for Aviation Safety, Fort Rucker, AL 36362 ATTN: Technical Library
1	Commander, Clarke Engineer School Library, 3202 Nebraska Ave., N, Fort Leonard Wood, MO 65473-5000 ATTN: Library
1	Commander, U.S. Army Engineer Waterways Experiment Station, P.O. Box 631, Vicksburg, MS 39180 ATTN: Research Center Library
1	Commandant, U.S. Army Quartermaster School, Fort Lee, VA 23801 ATTN: Quartermaster School Library
2	Naval Research Laboratory, Washington, DC 20375 ATTN: Dr. G. R. Yoder - Code 6384
1	Chief of Naval Research, Arlington, VA 22217 ATTN: Code 471
1	Commander, U.S. Air Force Wright Research & Development Center, Wright-Patterson Air Force Base, OH 45433-6523 ATTN: WRDC/MLLP, M. Forney, Jr.
1	WRDC/MLBC, Mr. Stanley Schulman
1	U.S. Department of Commerce, National Institute of Standards and Technology, Gaithersburg, MD 20899 ATTN: Stephen M. Hsu, Chief, Ceramics Division, Institute for Materials Science and Engineering

No. of Copies	To
1	Committee on Marine Structures, Marine Board, National Research Council, 2101 Constitution Avenue, N.W., Washington, DC 20418
1	Materials Sciences Corporation, Suite 250, 500 Office Center Drive, Fort Washington, PA 19034
1	Charles Stark Draper Laboratory, 555 Technology Square, Cambridge, MA 02139
	Wyman-Gordon Company, Worcester, MA 01601
1	ATTN: Technical Library
	General Dynamics, Convair Aerospace Division, P.O. Box 748, Fort Worth, TX 76101
1	ATTN: Mfg. Engineering Technical Library
	Plastics Technical Evaluation Center, PLASTEC, ARDEC, Bldg. 355N, Picatinny Arsenal, NJ 07806-5000
1	ATTN: Harry Pebly
1	Department of the Army, Aerostructures Directorate, MS-266, U.S. Army Aviation R&T Activity - AVSCOM, Langley Research Center, Hampton, VA 23665-5225
1	NASA - Langley Research Center, Hampton, VA 23665-5225
	U.S. Army Vehicle Propulsion Directorate, NASA Lewis Research Center, 2100 Brookpark Road, Cleveland, OH 44135-3191
1	ATTN: AMSRL-VP
	Director, Defense Intelligence Agency, Washington, DC 20340-6053
1	ATTN: ODT-5A (Mr. Frank Jaeger)
	U.S. Army Communications and Electronics Command, Fort Monmouth, NJ 07703
1	ATTN: Technical Library
	U.S. Army Research Laboratory, Electronic Power Sources Directorate, Fort Monmouth, NJ 07703
1	ATTN: AMSRL-EP-M, W. C. Drach
1	AMSRL-EP-M, T. E. Koscica
1	AMSRL-EP-M, R. W. Babbitt
	Director, U.S. Army Research Laboratory, Watertown, MA 02172-0001
2	ATTN: AMSRL-OP-CI-D, Technical Library
20	Authors